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著者別表示	小村 和久
journal or publication title	Journal of Nuclear and Radiochemical Sciences
volume	9
number	2
page range	49-52
year	2009-01-01
URL	<a href="http://doi.org/10.24517/00029305">http://doi.org/10.24517/00029305</a>

doi: <https://doi.org/10.14494/jnrs.9.49>



# Some Applications of the Gold Activation by Environmental Neutrons

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## **Abstract**

The activation of gold by environmental neutrons was used to study the effect of concrete buildings at our laboratory (LLRL) on the neutron flux, and to estimate the thermal neutron flux in and around the building of Kinki University Training Reactor (UTR-Kinki). The results showed that three ceilings of thickness (34 g/cm<sup>2</sup> each) decrease the fast neutrons to 26 %. However, the same reinforced concrete decreases the slow flux to only 62 %.

On the other hand, the thermal neutron flux at 283m from the reactor center was two times higher than the environmental background. These results can give attention to the effect of concrete walls as a shielding around the reactors, especially those that have been hold near to the living environments.

*Keywords: Environmental neutrons; activation of gold; thermal and fast neutrons; concrete; reactors.*

## 1. Introduction

The vertical cut-off of geomagnetic rigidity and the change of geographical latitudes affect the distribution of the secondary cosmic radiation including neutrons. However, at sea level and its vicinity, the measured neutron data are more affected by the meteorological conditions.<sup>1,2</sup> The primary cosmic ray interacts with all materials to produce secondary cosmic neutrons. The background measurements at sea and land were made up of neutrons produced, attenuated, reflected, and absorbed by air, water, or ground<sup>2</sup>. The meteorological data includes air pressure, overhead cloud-amounts, wind speed, precipitation, and water contents. This means that, the air-ground boundary effects<sup>3</sup> on the spatial and energy distributions of the neutrons depend on greatly upon the type of local surroundings.<sup>4</sup>

The results of altitude dependence measurements of the environmental neutron flux made by Yousef<sup>5</sup> showed some difference between the measured neutron flux inside and outside the concrete buildings. This difference was appeared as a decrease of the measured flux inside the buildings comparing with that outside the buildings at the same altitude and position. The attention was directed to the effect of concrete. An advantage of the experiment is that the composition of the concrete can be taken as approximately that the earth with constant moisture contents.<sup>6</sup> Considering the effect of the concrete, this effect was more clearly at the high altitudes than the low altitudes for slow neutron flux.

As one of the most important applications of the gold activation by environmental neutrons is the study of the neutron flux in the environment around the strong neutron sources such as reactors, accelerators and so on. Around these sources, the neutrons contribute with great part of radiation doses to the workers in these facilities and the other surrounding circumstances.

## 2. Experimental technique

The environmental neutron measurements were carried out indirectly through the radioactivity induced in pure gold by neutron activation. Because of its suitable half-life (2.694 days) and high cross section ( $98.5 \pm 0.4$  barn) for thermal neutrons, the  $^{198}\text{Au}$  was the most convenient neutron detector as a product of  $^{197}\text{Au}(n,\gamma)^{198}\text{Au}$  interaction with 100 % abundance. The  $\beta$ -decay of  $^{198}\text{Au}$  occurs with the emission  $\gamma$ -rays with 411.8 keV (95.56 %). The  $\gamma$ -ray measurements were made using an extremely low-background gamma-ray counting system constructed in the tunnel of former Ogoya Copper Mine (270 mwe depth).<sup>7</sup> After neutron exposure, the targets were wrapped with cadmium sheets and brought back to laboratory as early as possible to start  $\gamma$ -ray measurements. The 411.8 keV  $\gamma$ -ray from  $^{198}\text{Au}$  was measured to calculate the number of  $^{198}\text{Au}$  atoms produced in unit weight of gold and then converted to the neutron flux using the three-dimensional *Monte Carlo Code MORSE-CG*.<sup>8</sup>

## 3. Sampling

To study the effect of concrete buildings on the environmental neutron flux, the experiments were mainly conducted in a 3-storied concrete building of Low Level Radioactivity Laboratory (LLRL). As seen in Figure 1, data were taken at each floor, as well as the roof of the building. Three targets of 50g gold grains inside 8.5-cm paraffin thickness were exposed at 1<sup>st</sup>, 2<sup>nd</sup> floor and roof of LLRL. In addition, twelve gold targets of 20g grains were distributed during the roof and the three floors of the building. Four target sets composed of bare, Cd (0.5 mm) covered and paraffin covered (7.5cm thick) were exposed at every point with 80 cm distance to avoid interaction. The black circles refer in Figure 1 show the

position of the targets in the first experiment, while the open circles represent the second experiment. As a point of notification, the 2<sup>nd</sup> floor-target has only one concrete ceiling in the first measurements as it shown in Figure 1. The thickness of every reinforced-concrete layer was estimated to be about  $34 \text{ g cm}^{-2}$ .

On the other hand, at Kinki University Training Reactor (UTR-Kinki), 25 gold sheet targets were divided to 5 groups to estimate the thermal neutron flux intensity in and around the reactor building (Figure 2). The first group consisted of 4 targets, which were exposed inside the reactor body for one-hour operation. Two of these targets were placed in the core of the reactor and the other two were placed at 20 cm above the core. One target at each place was covered with 0.5 mm Cd sheet to estimate the Cd ratio in the high intensity flux. The targets were cooled for 17 days before  $\gamma$ -ray measurement this was because of their high radioactivity level. The targets of the second group were distributed inside the reactor room at four different distances from the reactor center. This group was exposed for one hour only during the reactor operation to estimate the thermal flux around the reactor body during the operation. After 24 h cooling, the  $\gamma$ -ray of targets was measured by Ge-detectors. The targets of the third group were exposed at the same points of the second group for one week to evaluate the average neutron flux intensity over one week operation. This group consisted of four bare targets in addition to two targets with Cd cover. Another five gold targets were distributed inside the reactor building to represent the 4<sup>th</sup> group. This group was placed to evaluate the intensity of the thermal neutron flux with which the workers are exposed for one week. The last group consisted of 6 targets, which were distributed outside the reactor building until 283 m distance to estimate the thermal neutron flux in the reactor environment and to evaluate the runaway neutrons

from the reactor to the surrounding environment. Two of these targets were placed together at the far point. This group was exposed for one week, except for one of the couple targets, which was left for one-month exposure to compare with the other target.

All targets were wrapped in Cd sheets during the cooling time. The short exposure and cooling times were corrected during the calculations of the production of gold atoms (N) using the known equation (1) .

$$N = \frac{C}{\varepsilon} \frac{1}{1 - \exp(-\lambda t_R)} \frac{1}{\exp(-\lambda t_D)} \frac{1}{1 - \exp(-\lambda t_C)}$$

$$A = \lambda N \dots\dots\dots(1)$$

Where A is the reaction rate of radionuclide  $^{198}\text{Au}(n,\gamma)$

$\lambda$  is the decay constant of the radionuclide  $^{198}\text{Au}$ ,

C is the peak count,

$\varepsilon$  is the peak efficiency,

$t_R$  is the irradiation (exposure) time,

$t_D$  is the decay (cooling) time before counting,

and  $t_C$  is the counting (measuring) time.

## 4. Results and discussion

### 4.1 Influence of concrete buildings on the environmental neutron flux

Tables 1 and 2 and Figure 3 depict the results of the concrete effect experiments at LLRL. The effect of reinforced concrete is clearly observed from these results. The neutron fluxes were gradually decreased from the roof to the 1<sup>st</sup> floor exponentially. The fast neutron flux at the 1<sup>st</sup> floor showed 36% and 26% from its values at the roof in the first and second experiments, respectively. As a

comprehensive estimation, the second experiment is the more interesting for discussion. Although in the fast neutrons measurement, the reduction ratio of 3<sup>rd</sup> floor / roof and 1<sup>st</sup> floor / 2<sup>nd</sup> floor was constant, about 13 %, this ratio increased to 47 % for 2<sup>nd</sup>/3<sup>rd</sup> floor. The cause of this high reduction is due to the thermalization of the fast neutron by the interaction or scattering with the component of the library, such as aluminum shelves, books, and so on, where the targets were placed.

Cadmium measurements have a similar behavior like the fast neutrons because its value depends mainly on the epithermal flux. On the other hand, the slow neutron flux showed a different behavior. The reduction ratio of 3<sup>rd</sup> floor/roof was about 19 % and 13 % for 2<sup>nd</sup> floor/3<sup>rd</sup> floor, respectively. This ratio decreased to 6% for 2<sup>nd</sup> floor/1<sup>st</sup> floor. The reduction at the 3<sup>rd</sup> floor came from the concrete effect, however, in the 2<sup>nd</sup> and 1<sup>st</sup> floors values, the absorbed slow flux by concrete is compensated by the thermalization of the high energy flux by the concrete and the other components and furniture of the building.

The Cd ratio increased gradually from 3.4 at the roof to 9.4 at the 1<sup>st</sup> floor, this means that the thermal neutrons are the most predominant than the epithermals at lower floors. This effect is a result of the thermalization of fast neutrons by the concrete.

From these results, it is evident that the concrete is an effective shield for the high-energy neutrons. Three ceilings of 34 g cm<sup>-2</sup> thickness decreased the flux to 26 % from its original value. However, the same reinforced concrete decreased the slow flux to only 62 % from its original value. These results can give attention to the effect of concrete walls as a shielding around the reactors, especially those that have been hold near to the living environments.

## 4.2 Estimation of the thermal neutron flux around the Kinki University Reactor

The thermal neutron flux intensity was estimated inside and around a research reactor. The neutron source for starting the reactor is Pu-Be (37 GBq). The estimated thermal flux at the core of the reactor is  $1.2 \times 10^7 \text{ n cm}^{-2} \text{ s}^{-1}$  and  $1.2 \times 10^5 \text{ n cm}^{-2} \text{ s}^{-1}$  at 20 cm over the core. On the other hand, the fast neutron is  $1.3 \times 10^6 \text{ n cm}^{-2} \text{ s}^{-1}$  at the core. According to Prof. Morishima, Cd ratio is estimated to be 5~7 at the core of the reactor.

Table 3 shows the results of one-hour exposure targets. The thermal neutron flux at the core of the reactor is  $1.24 \times 10^7 \text{ n cm}^{-2} \text{ s}^{-1}$  and  $5.25 \times 10^5 \text{ n cm}^{-2} \text{ s}^{-1}$  at 20 cm above the core. The Cd ratio at the two points is 13.4 and 13.6, respectively. These results are about 2 times higher the ratio than the official value. The large values of the present data may be caused by the thick of Cd (0.5 mm) sheet used for covering gold target or target position was higher than bare gold experiment. The epithermal neutrons are reflected and moderated from the fast neutron by the components of the reactor or the moderator. The results around the reactor body showed no clear relation between the flux intensity and the distance from the reactor. This is due to the target position in respect to the enriched uranium source. Hence, the targets were placed at 3.1 m over the reactor. The others were set beside the wall of the reactor body or steel door or the concrete outer wall. So, the adjacent material may have some effect on the neutron flux. This effect is more clearly at 5.7 m where the targets number 8~10 were stock to steel door. Hence, the thermal neutron production over steel bodies is about 11 times higher than the environmental background.<sup>9)</sup> This is due to the marked rises of the flux at that point. The average thermal flux inside the reactor



room was about  $77.6 \pm 3.5 \times \text{n cm}^{-2} \text{s}^{-1}$  over the reactor and on an average  $15.2 \pm 2.3 \text{ n cm}^{-2} \text{s}^{-1}$  around the reactor room.

Table 4 shows that the thermal neutron flux measured for one week at the same points has the same behavior except that its intensity was distributed over one week exposure. This means that the measured results for one hour are correct. The average of the slow flux intensity over one week decreased to  $3.35 \pm 0.18 \text{ n cm}^{-2} \text{s}^{-1}$  and  $0.68 \pm 0.16 \text{ n cm}^{-2} \text{s}^{-1}$  over and around the reactor, respectively. These results show that the exposure for one week decreased the average flux intensity to 4.3 % and 4.5 % over and around the reactor, respectively, comparing with its value during the operating. The Cd ratio at 3.1 and 5.7 m was 8.2 and 8.4, respectively. Comparing these ratios with those obtained inside the reactor body shows that the Cd-shield is more effective at high intensity flux.

The thermal neutron flux distribution inside the reactor room is plotted together with the flux inside the building in Figure 4 to show the variation of the intensity with the distance from the reactor center. This figure shows obviously that the intensity of the thermal flux decreases exponentially with the distance from the reactor. These results indicate that the thermal neutron flux inside the control room, where the workers spend most the time during the operating of the reactor, was about  $0.41 \pm 0.04 \text{ n cm}^{-2} \text{s}^{-1}$ . This value was measured by targets number 13. The average of the corresponding values in the hall was about  $0.080 \pm 0.04 \text{ n cm}^{-2} \text{s}^{-1}$ . This value decreased to  $0.034 \pm 0.008 \text{ n cm}^{-2} \text{s}^{-1}$  at the entrance of the building.

Although Figure 4 shows also that the thermal neutron flux decreases gradually with the distance outside the reactor building, the flux is still higher than the environmental background level. The marked increase of the flux at 40 m and 70 m is due to that the

targets which were placed inside aluminum boxes, where the production of the neutron flux is about 3 times higher than the environmental background. The drop of the flux at 140m distance is due to the effect of much concrete buildings around the workshop station, where the target was placed.

The thermal neutron flux at 283m was measured to be  $(16.0 \pm 1.6) \times 10^{-3} \text{ n cm}^{-2} \text{ s}^{-1}$ , which is two times higher than environmental neutron  $(7.2 \pm 0.6) \times 10^{-3} \text{ n cm}^{-2} \text{ s}^{-1}$ . In order to confirm this anomaly 2<sup>nd</sup> measurement was made, however the flux was measured to be  $(15.4 \pm 2.6) \times 10^{-3} \text{ n cm}^{-2} \text{ s}^{-1}$ . This result shows the stability of the environmental neutron flux over the average of all the time.

From this Figure 4 it is evident that the thermal neutron flux is rapidly decrease with the increase of the distance from the reactor center. This effect is due to the interaction or absorption of the thermal neutrons with or by the air, concrete buildings and the other surrounding materials. Also the figure shows obviously that the rise of the environmental neutron flux in the environment around the reactor is caused by the diffusion of the reactor neutrons or sky shine effect.

### **Acknowledgement**

The authors wish to express deep thanks to Dr. T. Imanaka, Associate Prof. at Kyoto Univ. for his kind help to calculate the results by Monte Carlo code programs. Also, to all members of UTR-Kinki especially Prof. Morishima, UTR-Kinki and to Mr. H. Kofuji, LLRL (Kanazawa Univ.) for their grateful help during the UTR-experiments.

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#### Table caption and figure caption

Table 1. Environmental fast neutron flux measured at different floor at LLRL.

Table 2. Environmental neutron fluxes measured at different floor at LLRL.

Table 3. Results of neutron flux measurement exposed for one hour operation of the reactor at 1Watt.

Table 4. Average neutron flux in and around the reactor building during one week operation.

#### Figure captions

Figure 1. Target set positions at LLRL.

Figure 2 Target set positions at UTR-Kinki

Figure 3. Slow neutron, fast neutron and Cd covered flux at LLRL.

Figure 4 Slow neutron flux inside and outside the building of UTR-Kinki .

Tabpe 1. Fast neutron flux at LLRL (Exp.1).

Exposure elevation	Au-198 atom/g			Neutron flux (n/cm <sup>2</sup> /s)X10 <sup>-3</sup>			Reduction ratio / floor
Roof	75.7	±	10.5	1.95	±	0.27	1
2nd floor	57.5	±	10.6	1.48	±	0.27	0.76
1st floor	27.2	±	7	0.7	±	0.18	0.36

Table 2

Exposure Condition	Exposure elevation	$^{198}\text{Au}$ (arom/g)	Neutron flux (n/cm <sup>2</sup> /s)X10 <sup>-3</sup>	Reduction ratio / floor	Cadmium ratio
Slow neutron (Bare)	Roof	51.6 ± 8.4	7.70 ± 1.24	1.00	
	3rd floor	41.5 ± 9.6	6.20 ± 1.43	0.81	
	2nd floor	34.9 ± 10.1	5.20 ± 1.50	0.68	
	1st floor	32.4 ± 7.4	4.80 ± 1.10	0.62	
Fast neutron (Parrafin)	Roof	102 ± 6.2	1.97 ± 0.31	1.00	
	3rd floor	88.4 ± 14.6	1.70 ± 0.28	0.86	
	2nd floor	39.9 ± 8.9	0.77 ± 0.17	0.39	
	1st floor	26.2 ± 7.7	0.51 ± 0.15	0.26	
Cadmium measurements (Cd)	Roof	15.1 ± 4.6	3.20 ± 1.00	1.00	3.4 ± 1.2
	3rd floor	10.6 ± 4.1	2.30 ± 0.88	0.72	3.9 ± 1.7
	2nd floor	5.74 ± 3.4	1.40 ± 0.73	0.44	6.1 ± 4.0
	1st floor	3.46 ± 3.1	0.75 ± 0.67	0.23	9.4 ± 8.6

Table3

Target No.	Condition	Distance from R. Center (m)	$^{198}\text{Au}$ ( atom / g)	Thermal neutron flux (n/cm <sup>2</sup> /s)	Cd ratio
Inside the Reactor					
A 1	Bare	0	1.10E+11 ±	1.24E+07	
A 2		0.2	4.90E+09 ±	5.52E+05	
A 3	Cd	0	8.20E+09 ±	1.78E+06	13.4
A 4		0.2	3.60E+08 ±	7.81E+04	13.6
Inside the reactor room					
6	Bare	1.9	1.18E+05 ± 1.5E+04	13.3 ± 1.6	
3		3.1	6.89E+05 ± 3.1E+04	77.6 ± 3.5	
11		5.2	1.30E+05 ± 1.2E+04	14.6 ± 1.3	
8		5.7	1.58E+05 ± 1.6E+04	17.8 ± 1.8	





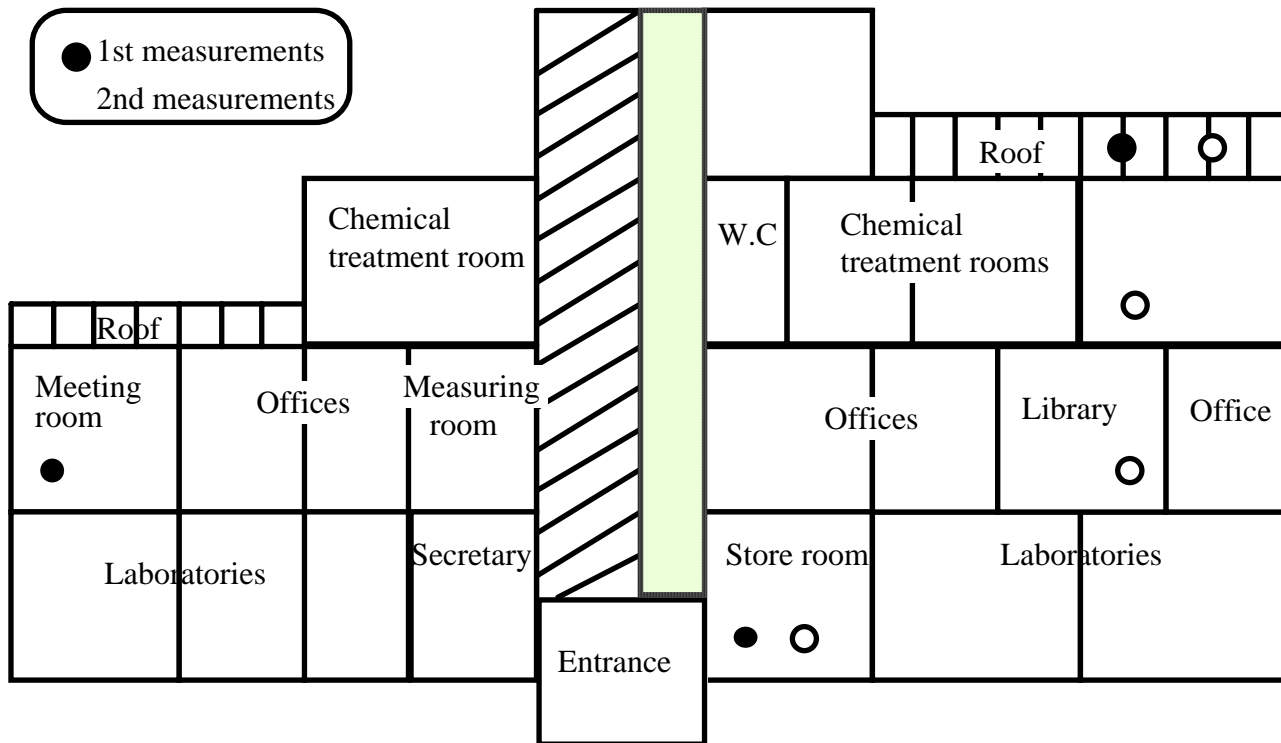


Fig. 1 Target setting position at LLRL

