

# Numerical modeling on thermal interaction between thermal plasma and solid powder for materials processing

メタデータ	言語: eng 出版者: 公開日: 2020-01-09 キーワード (Ja): キーワード (En): 作成者: メールアドレス: 所属:
URL	<a href="http://hdl.handle.net/2297/00056493">http://hdl.handle.net/2297/00056493</a>

This work is licensed under a Creative Commons Attribution-NonCommercial-ShareAlike 3.0 International License.



# **DISSERTATION ABSTRACT**

**NUMERICAL MODELING ON  
THERMAL INTERACTION BETWEEN THERMAL PLASMA AND  
SOLID POWDER FOR  
MATERIAL PROCESSING**



**KANAZAWA UNIVERSITY**  
GRADUATE SCHOOL OF NATURAL SCIENCE AND TECHNOLOGY  
ELECTRICAL ENGINEERING AND COMPUTER SCIENCE

STUDENT ID 1624042016

**YULIANTA SIREGAR**

CHIEF ADVISOR  
PROF. YASUNORI TANAKA

JUNE, 2019



# Contents

Acknowledgement . . . . .	xv
Chapter1 Introduction . . . . .	3
1.1 Plasma state . . . . .	3
1.1.1 Overview of plasma . . . . .	3
1.1.2 Concept of temperature in a plasma . . . . .	4
1.1.3 Different types of plasma by temperature . . . . .	6
1.2 Inductively coupled thermal plasma torch . . . . .	9
1.3 Objective of this thesis . . . . .	11
1.4 Composition of the thesis . . . . .	13
References in chapter 1 . . . . .	15
Chapter2 Influence of input power in Ar/H <sub>2</sub> thermal plasma with Si powder by simulation . . . . .	19
2.1 Introduction . . . . .	19
2.2 Configuration of Inductively Coupled Thermal Plasma torch . . . . .	20
2.3 Modeling of the Inductively Coupled Thermal Plasma with Powder Injection	21
2.3.1 Modelling Assumptions . . . . .	21
2.3.2 Governing equation . . . . .	22
2.3.3 Calculation condition . . . . .	24
2.4 Calculation results . . . . .	26
2.4.1 The Temperature Distribution of Thermal Plasma . . . . .	26
2.5 Summary of chapter 2 . . . . .	33
References in chapter 2 . . . . .	35
Chapter3 Numerical Parametric Investigation on Temperature Distribution in Ar/O <sub>2</sub> Induction Thermal Plasmas with Ti Powder Injection -Inclusion of Particle Evaporation- . . . . .	39

---

3.1	Introduction . . . . .	39
3.2	Configuration of inductively coupled thermal plasmatorch . . . . .	41
3.3	Modeling . . . . .	43
3.3.1	Assumptions . . . . .	43
3.3.2	Governing equation for Ti particle . . . . .	44
3.3.3	The drag force coefficient and heat transfer coefficient . . . . .	46
3.3.4	Governing equation for thermal plasma region . . . . .	47
3.3.5	Interaction between Ti particle and thermal plasma . . . . .	49
3.3.6	Thermodynamic properties of Ar/O <sub>2</sub> mixture and Ti vapor . . . . .	50
3.3.7	Calculation condition . . . . .	55
3.4	Calculation results . . . . .	58
3.4.1	Influence of operation parameters reduced to lower values . . . . .	58
3.4.2	Influence of operation parameters increased to higher values . . . . .	64
3.4.3	Particle behavior . . . . .	70
3.5	Summary of chapter 3 . . . . .	75
	References in chapter 3 . . . . .	77
Chapter4	Numerical study of temperature and gas flow fields in Ar-O <sub>2</sub> tandem-type inductively coupled thermal plasma with Ti feedstock powder injection . . . . .	81
4.1	Introduction . . . . .	81
4.2	Configuration of Tandem-coil Induction Thermal Plasma Torch . . . . .	83
4.3	Modelling of Tandem-coil Induction Thermal Plasma . . . . .	86
4.3.1	Modelling assumptions . . . . .	86
4.3.2	Governing equation for Ti feed powder . . . . .	87
4.3.3	Governing equation for tandem-coil induction thermal plasma . . . . .	90
4.3.4	Interaction between Ti particles and tandem coil thermal plasma . . . . .	92
4.3.5	Thermodynamic and transport properties of Ti bulk, Ar-O <sub>2</sub> -Ti system . . . . .	95
4.3.6	Boundary condition . . . . .	96
4.3.7	Calculation conditions for single-frequency coil ICTP and tandem coil ICTP . . . . .	104
4.4	Calculation Results . . . . .	107

---

4.4.1	Temperature distribution of thermal plasma . . . . .	107
4.4.2	Mass fraction distribution of titanium vapour and gas flow pattern .	125
4.4.3	Particle behaviour . . . . .	134
4.5	Summary of chapter 4 . . . . .	139
	References in chapter 4 . . . . .	141
Chapter5	Conclusions . . . . .	145
5.1	Introduction . . . . .	145
5.2	Summary of results . . . . .	146
5.2.1	Influence of input power in Ar/H <sub>2</sub> thermal plasma with Si powder by simulation . . . . .	146
5.2.2	Numerical Parametric Investigation on Temperature Distribution in Ar/O <sub>2</sub> Induction Thermal Plasmas with Ti Powder Injection-Inclusion of Particle Evaporation- . . . . .	146
5.2.3	Numerical study of temperature and gas flow fields in Ar-O <sub>2</sub> tandem- type inductively coupled thermal plasma with Ti feedstock powder injection . . . . .	147
5.3	Future researches . . . . .	148



# List of Figures

1.1	States of materials. . . . .	4
1.2	Maxwell-Boltzmann distribution of velocities in argon atom. . . . .	5
1.3	Classification of plasmas by electron temperature and electron density. . .	7
1.4	Configuration of ICTP torch. . . . .	8
2.1	Configuration of ICTP torch. . . . .	20
2.2	The temperature distribution of 99% Ar-1% $H_2$ ICTPs with Si powder injection at input powers of 20 kW, 30 kW, and 40 kW. . . . .	27
2.3	Radial temperature distribution of 99% Ar-1% $H_2$ ICTP at an axial position of 250 mm with Si powder injection. . . . .	28
2.4	Axial temperature distribution of 99% Ar-1% $H_2$ ICTP at an radial position of 5 mm with Si powder. . . . .	28
2.5	Diameter variation for 35 kinds of Si particles injected with different 7 initial diameters and 5 different initial positions as a function of axial position in 99% Ar-1% $H_2$ ICTPs. . . . .	30
2.6	Mass fraction distribution of 99% Ar-1% $H_2$ ICTPs with Si powder injection at input powers of 20 kW, 30 kW and 40 kW. . . . .	31
2.7	Streamlines in 99% Ar-1% $H_2$ ICTPs with Si powder injection at input powers of 20 kW, 30 kW, and 40 kW. . . . .	32
3.1	Configuration of inductively coupled thermal plasma torch used in the calculation. . . . .	42
3.2	Initial positions of particle injections and particle size distribution. . . . .	43
3.3	Molar fraction of thermal plasma in 90%Ar+10% $O_2$ at a pressure of 300 Torr. . . . .	52
3.4	Molar fraction of thermal plasma in 89%Ar+9% $O_2$ +9%Ti at a pressure of 300 Torr. . . . .	52



---

3.5	Specific heat at constant pressure for Ar-O <sub>2</sub> thermal plasma with Ti vapor at a pressure of 300 Torr. . . . .	53
3.6	Electrical conductivity for Ar-O <sub>2</sub> thermal plasma with Ti vapor at a pressure of 300 Torr. . . . .	53
3.7	Viscosity for Ar-O <sub>2</sub> thermal plasma with Ti vapor at a pressure of 300 Torr.	54
3.8	Temperature distribution of Ar-O <sub>2</sub> thermal plasma with Ti powder injection for reduced sheath gas flow rate (a), feedstock feeding rate (b), input power (c) from the reference condition at a pressure of 300 Torr. . . . .	59
3.9	Radial temperature distribution of Ar-O <sub>2</sub> thermal plasma with Ti powder injection at axial positions of 250 mm for reduced sheath gas flow rate (a), feedstock feeding rate (b), input power (c) from the reference condition. . .	60
3.10	Axial temperature distribution of Ar-O <sub>2</sub> thermal plasma with Ti powder injection at radial positions of 5 mm for reduced sheath gas flow rate (a), feedstock feeding rate (b), input power (c) from the reference condition. . .	60
3.11	Streamline in Ar-O <sub>2</sub> thermal plasma with Ti powder injection for reduced sheath gas flow rate (a), feedstock feeding rate (b), input power (c) from the reference condition at a pressure of 300 Torr. . . . .	61
3.12	Mass fraction distribution of Ti vapor in Ar-O <sub>2</sub> plasma with Ti powder injection for reduced sheath gas flow rate (a), feedstock feeding rate (b), input power (c) from the reference condition at a pressure of 300 Torr. . .	63
3.13	Temperature distribution in Ar-O <sub>2</sub> thermal plasma with Ti powder injection for increased sheath gas flow rate (d), feedstock feeding rate (e), input power (f) from the reference condition at a pressure of 300 Torr. . . . .	65
3.14	Radial temperature distribution of Ar-O <sub>2</sub> thermal plasma with Ti powder injection for increased sheath gas flow rate (d), feedstock feeding rate (e), input power (f) at axial positions of 250 mm. . . . .	66
3.15	Axial temperature distribution of Ar-O <sub>2</sub> thermal plasma with Ti powder injection for increased sheath gas flow rate (d), feedstock feeding rate (e), input power (f) at radial positions of 5 mm. . . . .	66

---

3.16	Streamline in Ar-O <sub>2</sub> thermal plasma with Ti powder injection for increased sheath gas flow rate (d), feedstock feeding rate (e), input power (f) from the reference condition at a pressure of 300 Torr. . . . .	67
3.17	Mass concentration distribution of Ti vapor in Ar-O <sub>2</sub> thermal plasma with Ti powder injection for increased sheath gas flow rate (d), feedstock feeding rate (e), input power (f) from the reference condition at a pressure of 300 Torr. . . . .	69
3.18	Time variation in particle diameters of 35 Ti particles injected into Ar-O <sub>2</sub> ICTP for the reference condition. Particles have initial 5 different diameters. The different curves with the same initial diameter indicates the results of particle diameters injected at different initial 7 radial positions as indicated in Fig. 3.2. . . . .	72
3.19	An example of particle temperature history flying of a single Ti particle in Ar-O <sub>2</sub> ICTP under the reference condition. Temperatures for 3 shells in a single particle are indicated here. . . . .	73
3.20	Time variation in particle diameters of 35 Ti particles injected into Ar-O <sub>2</sub> ICTP with 0.5 g/min feeding rate. Particles have initial 5 different diameters. The different curves with the same initial diameter indicates the results of particle diameters injected at different initial 7 radial positions as indicated in Fig. 3.2. . . . .	74
4.1	Configuration ICTP torch with (a) 8-turn coil and (b) 12-turn coil. . . . .	85
4.2	Definition of (a) Single-frequency coil and (b) Tandem double-frequency coil. . . . .	87
4.3	Definition of parameters for temperature inside a titanium particle. . . . .	90
4.4	Particle size distribution and particle injection positions. . . . .	94
4.5	Number density of (a) 90%Ar-10%O <sub>2</sub> and (b) 89%Ar-10%O <sub>2</sub> -1%Ti thermal plasmas at a pressure of 300 Torr. . . . .	99
4.6	Specific heat of 100%Ar gas, 90%Ar-10%O <sub>2</sub> gas mixture, 89%Ar-10%O <sub>2</sub> -1%Ti gas mixture and 100%Ti vapor as a function of temperature at 300 Torr pressure. . . . .	100

---

4.7	Thermal conductivity of 100%Ar gas, 90%Ar-10%O <sub>2</sub> gas mixture, 89%Ar-10%O <sub>2</sub> -1%Ti gas mixture and 100%Ti vapor as a function of temperature at 300 Torr pressure. . . . .	101
4.8	Viscosity of 100%Ar gas, 90%Ar-10%O <sub>2</sub> gas mixture, 89%Ar-10%O <sub>2</sub> -1%Ti gas mixture and 100%Ti vapor as a function of temperature at 300 Torr pressure . . . . .	102
4.9	A full-set of boundary conditions. . . . .	103
4.10	Temperature distribution in Ar-O <sub>2</sub> single-frequency coil ICTP with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	109
4.11	Axial temperature distribution at radial position of 25 mm in Ar-O <sub>2</sub> single-frequency coil ICTP with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	110
4.12	Radial temperature distribution at axial position of 230 mm in Ar-O <sub>2</sub> single-frequency coil ICTP with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	111
4.13	Power density distribution in Ar-O <sub>2</sub> single-frequency ICTP with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	112
4.14	Temperature distribution in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	115

---

4.15	Axial temperature distribution at a radial position of 25 mm in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	116
4.16	Radial temperature distribution at an axial position of 230 mm in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	117
4.17	Power density distribution in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	118
4.18	Temperature distribution in Ar-O <sub>2</sub> tandem double-frequency ICTP by a 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	121
4.19	Axial temperature distribution at the radial position of 25 mm in Ar-O <sub>2</sub> tandem double-frequency ICTP by a 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	122
4.20	Radial temperature distribution at an axial position of 230 mm in Ar-O <sub>2</sub> tandem double-frequency ICTP by a 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	123

---

4.21	Power density distribution in Ar-O <sub>2</sub> tandem double-frequency ICTP by a 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	124
4.22	Mass fraction distribution of Ti vapour in Ar-O <sub>2</sub> single-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	126
4.23	Streamlines in Ar-O <sub>2</sub> single-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The coil is operated at an input power of 25 kW at a frequency of 450 kHz. . . . .	127
4.24	Mass fraction distribution of Ti vapour in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	130
4.25	Streamlines in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	131
4.26	Mass fraction distribution of Ti vapour in Ar-O <sub>2</sub> tandem double-frequency ICTP by a 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	132

---

4.27	Streamlines in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 12-turn coil with Ti powder injection at different gap lengths of (a) 20 mm, (b) 30 mm, (c) 40 mm, and (d) 60 mm. The upper coil is operated at an input power of 10 kW at a frequency of 450 kHz, while the lower coil is operated at 15 kW and 300 kHz. . . . .	133
4.28	Variation in diameters of 35 Ti particles in Ar-O <sub>2</sub> single-frequency ICTP by an 8-turn coil with 60 mm gap length. . . . .	136
4.29	Temperature history of Ar-O <sub>2</sub> in single-frequency coil ICTP with 60 mm gap length. . . . .	137
4.30	Variation in diameters of 35 Ti particles in Ar-O <sub>2</sub> tandem double-frequency ICTP by an 8-turn coil with 60 mm gap length. . . . .	138
4.31	Variation in diameters of 35 Ti particles in Ar-O <sub>2</sub> tandem double-frequency ICTP by 12-turn coil with 60 mm gap length. . . . .	138



# List of Tables

2.1	Thermodynamic Properties of Silicon Powder . . . . .	25
3.1	Thermodynamic properties of titanium powder . . . . .	56
3.2	Calculation condition with lower value in parameters from reference. . . . .	56
3.3	Calculation condition with higher value in parameters from reference. . . . .	57
4.1	Numerical conditions . . . . .	105
4.2	Thermodynamic properties of titanium powder [37]. . . . .	106





# Acknowledgement

I wish to express my higher gratitude and thankful to Prof. Yasunori Tanaka as my major professor. You always help me since the first day to answer my questions and concerns, large or small, and many valuable suggestions, discussions, support, personal guidance, and encouragement. I feel very privileged to have worked with him. Without his guidance, I would never have learned what I know about the thermal plasma, principles of plasma discharge and material processing, tandem thermal plasma technology, and I would certainly never have come this far. Thank you very much.

For finishing this thesis I am indebted to many people for their help in completing this study. First of all, I would like to thank my co-supervisor Prof. Yoshihiko Uesugi, Prof. Tatsuo Ishijima and Dr. Yusuke Nakano for many useful discussions and helps. To all members of the Electric Power and Environment Laboratory for answering my questions with concerns.

I would also like to thank to dean of Engineering Faculty and Head Departement of Electrical Engineering at University of Sumatera Utara, Indonesia, I sincerely appreciate their help as well. I am also thankful to all my friends of Dikti-Kanazawa University awardee in 2016 who also strive to finish their study. I hope we can continue being friend and support each other.

I am grateful to and for my wife and best friend, Nani Barorah Nasution who kept me motivated and support me during all the process, I hope we always remember how we strive and hold on to reach our dream. My most thankful is to my beloved son and daughter, Danish Juna Siregar and Dhakira Juna Siregar. I am nothing without your love and caring, both of you is the real true fighter, and I learn a lot from both of you. I know it must be hard in the beginning to learn and adapt to new culture and language, but both of you make me proud and always grateful to be your father. Thank you for being lovely children. I hope one day, I will back to Japan, to see you study here.

I thanks to my parents Rahim Siregar and Chairani Harahap, from them I learn that education can change path and mind, thank you for the inspiration and the work ethic you instilled in me, I will never be able to payback all the love you give and teach me. I thank to my father in law and mother in law Nasrun Naution and Yusnani Tambunan, for always support us. I thank my brothers (in-law) and sister (in-law) Irfan Siregar, Yenny Marlina, Cherry Siregar, Zainal Safri, Andy Siregar, Intan Suhaila, Dicky Zickrika Siregar, Faradilla Safitri Siregar and all my nephews for always being supportive and always care

Lastly, but the most influence I would like to thank Allah SWT, as written in Al-Quran Surah Al-Mujadalah verse 11 “ Allah will raise to high ranks those of you who believe and are endowed with knowledge. Allah is well aware of all that you do ” . I hope through this process, I will one of the person who Allah grant high ranks.

# Abstract

Thermal interaction between feed rate powder and thermal plasma was calculated using the developed numerical model for inductively coupled thermal plasma (ICTP) with particle injection. The interaction between feed powder and thermal plasmas is greatly important to consider the stable establishment of the ICTP and effective heating and evaporation of injected particles, for example, for particle synthesis. Injected particles are heated by thermal plasma, and they are melted and evaporated to contaminate the thermal plasma, which influences the thermal plasma properties. The ICTP model was used in this research because it has benefit of good repeatability and no contamination process. Interactions between ICTP and injected powder are very complicated to be understood only by related experiments. The developed numerical model solves mass, momentum and energy conservation equations of thermal plasmas as well as mass transport equation for evaporated materials. In addition, particle motions were derived by solving the lagrange equation of motion. The temperature distribution inside the particles and phase transition from solid, liquid to gas of the particles were also taken into account.

Furthermore, numerical simulation in inductively coupled thermal plasma was made on the temperature distribution in argon (Ar)+ hydrogen (H<sub>2</sub>) induction thermal plasma torch with silicon (Si) powder injection to obtain the temperature distribution and gas flow fields. The ICTP model was used in this research because it has benefit of good repeatability and no contamination process. The temperature distributions of thermal plasma and Si vapor distribution were compared at input powers of 20 kW, 30 kW, and 40 kW. Results indicated that higher input power increases the temperature of the thermal plasma with doughnut shape but it slightly enhances evaporation of the powder at the center axis of the plasma torch.

In addition, thermal interaction between titanium feedstock powder and thermal plasma was calculated using the developed numerical model for inductively coupled thermal plasma

(ICTP) with particle injection. The interaction between titanium powder and thermal plasmas is greatly important to consider the stable establishment of the ICTP and effective heating and evaporation of injected particles, for example, for particle synthesis. Injected particles are heated by thermal plasma, and they are melted and evaporated to contaminate the thermal plasma, which influences the thermal plasma properties. The developed numerical model solves mass, momentum and energy conservation equations of thermal plasmas as well as mass transport equation for evaporated materials. In addition, particle motions were derived by solving the Lagrange equation of motion. The temperature distribution inside the particles and phase transition from solid, liquid to gas of the particles were also taken into account. Finally, a parametric study was conducted to show the influence of different important physical parameters such as input power, sheath gas flow rate, and Ti powder feeding rate.

In this thesis, tandem ICTP is formed using two coil currents (upper coil and lower coil) in a single plasma torch, that was already developed for nanoparticle synthesis. The temperature distribution of the tandem ICTP and evaporation of feedstock Ti powder were obtained for different gap lengths between the upper and lower coil and coil turn numbers. Results indicate that increasing the gap length between the upper and lower coil produces two separately controlled high-temperature areas in tandem ICTP. This result suggests that tandem ICTP provides a temperature field that is favourable for particle evaporation of injected particles while maintaining ICTP in the upper region of the plasma torch for stable operation

## 学位論文審査報告書（甲）

## 1. 学位論文題目（外国語の場合は和訳を付けること。）

Numerical modeling on thermal interaction between thermal plasma and solid powder for materials processing（材料加工のための熱プラズマと固体粉末の間の熱相互作用に関する数値モデリング）

## 2. 論文提出者 (1) 所 属 電子情報科学 専攻

(2) 氏 名 ゆりあんな しれがー  
Yulianta Siregar

## 3. 審査結果の要旨（600～650字）

2019年8月6日に第1回学位論文審査委員会、同日に口頭発表、第2回審査委員会を開催し、慎重審議の結果、以下のとおり判定した。なお、口頭発表における質疑を最終試験に代えるものとした。

本論文は、材料プロセス用誘導熱プラズマと、そこに投入する固体粉体との間の熱的相互作用のモデリングに関する研究である。誘導熱プラズマはガス温度が10000 Kにも達する高温高気圧のプラズマである。この誘導熱プラズマに原料固体粉体を導入することで、原料を蒸発させ、さらにそれを冷却することでナノ材料を大量に得ることがなされている。この物理過程を把握するためには、様々な診断とともに数値モデリングすることが重要である。本論文では、誘導熱プラズマを電磁熱流体で、固体粒子をラグランジュ粒子としてモデル化している。熱プラズマ流内での固体粒子の運動と、プラズマからの熱伝達による粒子の温度変化、さらに粒子の熔融・蒸発を考慮している。誘導熱プラズマは電磁場からジュール発熱とローレンツ力を受け、これらが熱プラズマ温度と流れ場を決定する。さらに、粒子の蒸発蒸気が熱プラズマの温度分布・流速分布に影響する。そのため、これらを包括的に考慮し、熱プラズマの電磁熱流体解析と粒子の運動・蒸発とが収束するまで計算している。本論文では、開発したモデルを用いて、TiO<sub>2</sub> ナノ粒子生成に使用される Ar-O<sub>2</sub> 誘導熱プラズマと Ti 原料粉体との相互作用、Si ナノ粒子生成に使用される Ar-H<sub>2</sub> 誘導熱プラズマと Si 原料粉体との相互作用を明らかにしている。さらに「タンデム型誘導熱プラズマ」についてもモデリングし、原料粉体の効率的蒸発と誘導熱プラズマの安定動作とが同時に実現できることを明らかにしている。

以上、本研究は誘導熱プラズマによる材料プロセスの物理解明に貢献するものであり、本論文は、博士（工学）に値すると判定した。

## 4. 審査結果 (1) 判定（いずれかに○印） ○合格 ・ 不合格

(2) 授与学位 博士（工学）

## 5. 学位論文及び参考論文に不適切な引用や剽窃が無いことの確認

■ 確認済み（確認方法：iThenticate による）

□ 未確認（理由：）