Selective separation of arsenic species from aqueous solutions with immobilized macrocyclic material containing solid phase extraction columns

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1	Selective Separation of Arsenic Species from Aqueous Solutions with
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3	Columns
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6	Ismail M. M. Rahman, ^{*, 1, 2} Zinnat A. Begum, ¹ Masayoshi Nakano, ¹ Yoshiaki
7	Furusho, ³ Teruya Maki, ¹ and Hiroshi Hasegawa ^{*, 1}
8	
9	¹ Graduate School of Natural Science and Technology, Kanazawa University, Kakuma,
10	Kanazawa 920-1192, Japan
11	² Department of Chemistry, University of Chittagong, Chittagong 4331, Bangladesh
12	³ GL Sciences, Inc., Nishishinjuku 6-22-1, Shinjuku, Tokyo 163-1130, Japan
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19	*Author(s) for correspondence.
20	E-mail: I.M.M.Rahman@gmail.com (I.M.M. Rahman); hhiroshi@t.kanazawa-u.ac.jp (H.
21	Hasegawa).
22	Tel/ Fax: +81-76-234-4792

23 Abstract

24 A combination of solid phase extraction (SPE) columns was used for selective separation 25 of water-soluble arsenic species: arsenite, arsenate, monomethylarsonic acid (MMA) and 26 dimethylarsinic acid (DMA). The SPE columns, namely AnaLig TE-01 (TE-01), AnaLig 27 AN-01 Si (AN-01) and AnaLig As-01 PA (As-01), contain immobilized macrocyclic material 28 as the sorbent and commonly known as molecular recognition technology (MRT) gel. The 29 retention, extraction and recovery behavior of the MRT gel SPE columns were studied at pH 4-10. Fortified deionized water spiked with 100 µM of arsenic species were treated at the 30 flow rate of 0.2 mL min⁻¹. HNO₃ (1.0 and 6.0 M) was used as eluent to recover the retained 31 32 arsenic species from TE-01 and AN-01 SPE columns. Arsenic species retained in the As-01 column were eluted with HNO₃ (0.1 M) followed by NaOH (2.0 M). Likely interference from 33 the various coexisting ions (Na⁺, K⁺, Ca²⁺, Mg²⁺, Cl⁻, NO₃⁻, CH₃COO⁻, PO₄³⁻, SO₄²⁻, ClO₄⁻) 34 35 (10 mM) were negligible. Quantitative separation of As(III), As(V), MMA and DMA was 36 achieved based on the differences in extraction and recovery behavior of the MRT gel SPE 37 columns with pH for different arsenic species. Complexation between arsenic species and MRT gel is the core phenomenon of the proposed technique as the complexation of MRT 38 39 gels is expected to be stronger than the resin-based separation processes. MRT gel SPE 40 columns are advantageous as compared with other reported SPE columns in terms of its 41 performance with As(III). Effortless regeneration and unaltered separation performance of 42 the sorbent materials for more than 100 loading and elution cycles are other sturdy 43 characteristics to consider the MRT gel SPE columns for sensitive and selective arsenic 44 species separation.

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Keywords: Solid phase extraction; Molecular recognition technology gel; water-soluble
arsenic; selective separation; pH

48 **1.0 Introduction**

Arsenic, a ubiquitous toxic trace element, has raised a major toxicological and environmental concerns (WHO, 2001). The concentration levels, oxidation and binding states, ionic and molecular forms and metabolic pathways of As vary strongly in different environmental compartments, food chains and ultimately in humans (Mandal and Suzuki, 2002). Widespread human exposure to high levels of As is reported to occur via drinking water and contaminated water irrigated food causing both cancerous and non-cancerous health effects (Karim, 2000; Rahman et al., 2008).

56 Arsenite (oxidation state + III), arsenate (oxidation state + V), monomethylarsonic acid 57 (MMA) and dimethylarsinic acid (DMA) are common water-soluble arsenic species existing in natural water systems-a major pathway of arsenic ingestion to humans (Smedley and 58 Kinniburgh, 2002). Arsenic toxicity in human depends strongly on its chemical form. As(III) 59 60 is 10 times more toxic than $A_{S}(V)$ while almost 70 times more toxic than the methylated forms, MMA and DMA (Squibb and Fowler, 1983). As(III), having successive acid 61 62 dissociation constants (pK_a) of 9.2, 12.2 and 13.4, is not dissociated at neutral pH and is present as a neutral species. As(V) and MMA has a wide range of pK_a values [As(V): 2.2, 6.9, 63 11.5; MMA: 4.1, 8.7], and exist mainly as anionic species at almost all pH. DMA with a pK_a 64 65 value of 6.2 subsists as a cation in acidic medium (Committee on Medical and Biologic Effects of Environmental Pollutants, 1977). The United States Environmental Protection 66 Agency proposed a maximum contaminant level of 10 μ g L⁻¹ arsenic for the community 67 water systems (USEPA, 2002). Because of increasingly stringent environmental regulations, 68 69 selective and accurate measurement of arsenic species is required for precise monitoring and 70 understanding the extent of arsenic contamination.

In natural waters, As usually exists at trace levels and several techniques are proposed for
 selective quantification and speciation analysis of arsenic species at trace levels (Barra et al.,

73 2000; Munoz and Palmero, 2005; Terlecka, 2005; Kumar and Riyazuddin, 2007; Mays and 74 Hussam, 2009). Ion chromatography and high performance liquid chromatography separation 75 followed by sensitive detection such as inductively coupled plasma mass spectrometry 76 (Lintschinger et al., 1998; Bissen and Frimmel, 2000), atomic absorption spectrometry (AAS) with hydride generation interface (Hasegawa et al., 1999; Kumar and Riyazuddin, 2007) and 77 78 electrospray/nanospray mass spectrometry (Pergantis et al., 1997; Ritsema et al., 1998) are 79 some potential techniques. However, concerns related to the use of element-selective 80 detectors to interface the chromatographic methods limit the efficiency of these techniques 81 (Yu et al., 2003).

82 Separation and preconcentration of contaminant ions using solid sorbent materials, known 83 as solid phase extraction (SPE) systems, have increased in popularity since the 1980s (Hosten 84 and Welz, 1999). The technique has been developed as a cost- and time-saving alternative to 85 the traditional extraction techniques featuring the capability to interact with a variety of metal 86 ions including the fairly specific selectivity to a particular ion (Nickson et al., 1995; Ghaedi et al., 2008). Ion exchange resins (Leal et al., 2004; Jitmanee et al., 2005), silica gel bonded 87 88 with octadecyl functional groups (Pozebon et al., 1998), yeast immobilized on controlled 89 pore glass (Koh et al., 2005), activated alumina (Karthikeyan et al., 1999), open tubes knotted 90 reactors (Yan et al., 2002; Herbello-Hermelo et al., 2005), polytetrafluoroethylene turnings-91 packed micro-columns (Anthemidis et al., 2010) have been employed as SPE sorbent 92 material. One group of SPE materials includes the macrocyclic chelants, such as crown ethers, 93 immobilized on a silica or polymer support (Hosten and Welz, 1999). Ion-selective behavior 94 of SPE-type systems with immobilized macrocyclic materials has been mentioned for 95 preconcentration and separation of metals (Bradshaw et al., 1988; Izatt et al., 1994; 96 Hasegawa et al., 2010). SPE techniques have been applied for the quantitative 97 analysis/speciation/separation of various trace elements including arsenic (Yalcin and Le,

98 2001; Yu et al., 2003; Liang et al., 2004; Long et al., 2006; Sanchez et al., 2009). Reports on 99 the retention behavior of different arsenic species with some SPE systems (silica-based or resin-based) at pH 5.5 (Yalcin and Le, 2001) and pH 5.6 (Yu et al., 2003) were available. It 100 101 was observed that the hydrophobic interaction of the arsenic species with the SPE materials, pK_a values and ionic characters are important factors which may control the retention 102 103 efficiency of the SPE columns (Yu et al., 2003). Though quantitative retention was achieved 104 with the SPE columns for the water-soluble arsenic species (As(III), As(V), MMA and 105 DMA), elution of the retained species was quiet difficult or sometimes unachievable for some 106 species particularly with As(III) (Yalcin and Le, 2001; Yu et al., 2003).

107 The objective of the work is to investigate the feasibility of an ion-selective immobilized 108 macrocyclic material attached to a solid phase, commonly known as a molecular recognition 109 technology (MRT) gel, for the selective separation of As(III), As(V), MMA and DMA from 110 aqueous solutions followed by graphite furnace AAS determination. We used following MRT 111 gel SPE columns: AnaLig TE-01, AnaLig AN-01 Si and AnaLig As-01 PA. Specific MRT 112 gel SPE columns have the advantage of the selective retention of the mentioned arsenic 113 species followed by quantitative recovery. Most importantly, As(III) was quantitatively 114 retained and recovered with the AnaLig As-01 PA SPE column.

115 **2.0 Experimental**

116 2.1 Instruments

A PerkinElmer model AAnalyst 600 AAS (PerkinElmer, Massachusetts, USA) including the AS-800 autosampler equipped with a transverse-heated graphite atomizer with integrated, pyrolytic graphite coated platform (THGA) and longitudinal Zeeman-effect background corrector was used. End-capped THGA tubes were used for better sensitivity and improved precision. An electrodeless discharge lamp (EDL) powered by EDL System II operated at 122 380 mA was employed as light source. The wavelength was set at the 193.7 nm resonance 123 line and the monochromator spectral bandpass at 0.7 nm. Baseline offset correction time was 124 set to 2.0 s and the read delay at 0.0 s. Argon was used as purge gas and the flow rate was set to 250 mL min⁻¹. A temperature program was performed and the different steps were: first 125 126 and second dry at 110 and 130 °C, ashing at 1200 °C and atomization at 2000 °C held at 30, 127 30, 20 and 5 s respectively. After a calibration with 5 standards (0.5-2.5 µM), 20 µL of 128 sample and 10 µL of Pd–Mg matrix modifier were introduced in the graphite furnace with 129 three replicates of each measurement. The pH of the sample solutions was measured with a 130 Navi F-52 pH meter (Horiba Instruments, Japan) and a combination electrode.

131 2.2 Reagents and materials

Analytical grade commercial products were used. Stock solutions (10 mM) of As(III), As(V), MMA and DMA were prepared from sodium arsenite (NaAsO₂) (Kanto Chemical, Japan), sodium arsenate heptahydrate (Na₂HAsO₄·7H₂O), monomethylarsonic acid (CH₃AsO(OH)₂), dimethylarsinic acid sodium salt trihydrate (C₂H₆AsNaO₂·3H₂O) (Nacali Tesque, Japan). Working standards of metal solutions in the range of μ M to mM were prepared by dilution on a weight basis. Deionized water prepared with a Barnstead 4 housing E-Pure systems was used to prepare all solutions and is referred to as EPW hereafter.

The experimental pH range was 4–10, and adjusted using either 1 M HCl or 1 M NaOH. MES (2-(*N*-morpholino) ethanesulfonic acid monohydrate, $C_6H_{13}NO_4S\cdot H_2O$) (Sigma–Aldrich, USA), HEPES (N-2-Hydroxyethylpiperazine-N'-2-ethanesulfonic acid, $C_8H_{18}N_2O_4S$) (Nacali Tesque, Japan), and TAPS (N-Tris(hydroxymethyl)methyl-3-aminopropanesulfonic acid, $C_7H_{17}NO_6S$) (MP Biomedicals, USA) were used as buffer reagents for pH 4–6, 7–8 and 9–10, respectively.

145 NaCl, KCl, CaCl₂, MgCl₂ were used as a source of cations while the Na-salt of anions 146 (Cl⁻, NO₃⁻, CH₃COO⁻, PO₄³⁻, SO₄²⁻, ClO₄⁻) (Nacali Tesque, Japan) were used to study the effect of coexisting ions. Working solutions of 10 mM concentration were prepared in H_2O matrix and pH was maintained to 7.0. The final solutions were allowed to equilibrate for 24 h before use. The interference study were carried out in a non-competitive environment by applying 4 mL of fortified deionized water at the optimized flow rate with subsequent collection using appropriate eluent.

Experimental variables, *e.g.* sample loading flow rate, selection of eluent and eluent concentration were optimized using As(V) spiked solutions (100 μ M) in H₂O matrix with pH maintained at 5.0. The MRT gel SPE columns were fed with 4 mL of sample solutions at varying flow rates, and the retention percentage of the As-species into the columns was determined. Different eluent (individual or combinations), 0.1–6.0 M HNO₃ and 0.1–4.0 M NaOH, was checked to select the most appropriate eluent or eluent combinations that were suitable for optimum recovery of the 'captured' species.

159 Certified reference materials (CRMs): BCR-713 (effluent wastewater) and BCR-610 160 (groundwater) from EC-JRC-IRMM (European Commission Joint Research Centre, Institute 161 of Reference Materials and Measurements), fortified samples of 'real' waters: tap water 162 sample from our laboratory in Kakuma campus, Kanazawa University (Kanazawa, Japan) 163 and river water sample from Asano River (Kanazawa, Japan) were analyzed to validate the 164 proposed separation process. Each of the real water samples was filtered through the cellulose 165 membrane filter of 0.45 μm pore size (Advantec, Japan) before the analysis.

Low-density polyethylene bottles (Nalge, USA), perfluoroalkoxy (PFA) tubes and micropipette tips (Nichiryo, Japan) were used throughout. The laboratory wares were cleaned following the sequence: (a) soaking in an alkaline detergent (Scat 20X-PF, Nacali Tesque, Japan) overnight, (b) rinsed with EPW, (c) soaking in 4 M HCl overnight, and (d) rinsed with EPW. PFA tubes and micropipette tips were cleaned according to the procedure described by Sohrin et al. (1998).

172 **2.3** Separation procedure

173 2.3.1 Column cleaning and conditioning

MRT gel SPE columns: AnaLig TE-01 (TE-01), AnaLig AN-01 Si (AN-01), AnaLig As-01 PA (As-01) were purchased from GL Sciences, Japan. The SPE sorbents are proprietary polymeric organic materials comprised of ion-selective sequestering property. The sorption ability of the SPE materials is based on the molecular recognition and macrocyclic chemistry. SPE materials packed in 3 mL columns were used in the experiments. Column cleaning was conducted with 8 mL of 1.0 M HNO₃ and 6 mL of EPW. Appropriate buffer solution (5 mL) was allowed to follow through the column to ensure the desired pH condition (4–10).

181 2.3.2 Retention, extraction and recovery of arsenic species with MRT gel columns

182 The work-flow sequence for the separation of As(III), As(V), MMA and DMA using 183 MRT gel SPE columns followed by GF-AAS determination is summarized in Table 1. 184 Sample solution (4 mL) was passed through the SPE column at the optimized pre-set flow rate of 0.2 mL min⁻¹. The pH of the sample solution was pre-adjusted with 0.1 M buffer 185 186 solution (MES, HEPES or TAPS, whichever appropriate). The column effluent was collected. 187 The MRT gel SPE columns were then washed with EPW to remove the analyte that is not 188 captured by the immobilized macrocyclic material in SPE columns. The total analyte 189 concentration in the column effluent and EPW wash solution represent the unretained 190 concentration of analyte in the SPE system. The final step is the elution of analyte from the 191 SPE systems. HNO₃ (1.0 and 6.0 M) was used to elute the arsenic species retained in TE-01 192 and AN-01 SPE columns, and analytes retained in As-01 column were eluted with 0.1 M 193 HNO₃ followed by 2.0 M NaOH. The arsenic concentrations in the sample, effluents and 194 eluent solutions were measured with GF-AAS. Three replicate measurements per sample 195 were made in all instances. The peak height of the reported signal was proportional to the 196 concentration of the respective arsenic species and was used for all measurements.

197 The terms, retention, extraction and recovery, were used to explain the separation 198 performance of the SPE systems. The retention ratio was calculated comparing the analyte 199 concentration in the sample solution loaded in SPE columns with that in the solution passed 200 through the columns providing only the information about the concentration of analyte sorbed in the SPE systems. On the other hand, the analyte concentrations in the column effluent, 201 202 EPW wash solution and eluent were measured to understand the extraction and recovery behavior of the SPE columns. The extraction ratio of each column for the individual species 203 204 was calculated by comparing the numbers of mol of analyte in the eluent with the cumulative 205 number of mol of analyte present in the total effluents. Numbers of mol of analyte recovered 206 in all fractions were compared with the numbers of mol of analyte in the solution loaded to 207 the column to calculate the recovery ratio.

208 **3.0 Results and discussion**

209 3.1 Optimization of variables

210 3.1.1 Sample loading flow rate

211 The flow rate of the metal-rich sample solution has a reasonable impact on the metal retention rate in SPE columns (Bag et al., 1998). Effect of sample loading flow rates adjusted 212 in the range of 0.2-4.0 mL min⁻¹ (Table 2) was checked at the optimum conditions. 213 Quantitative retention up to the flow rates of 0.25 mL min^{-1} was observed. The retention 214 capacities decrease gradually with the increase of flow rates above 0.25 mL min⁻¹. Such 215 behavior indicates the constant retaining capability of the MRT gel at the initial loading 216 period. Therefore, a flow rate of 0.2 mL min⁻¹ was applied to ensure maximum retention of 217 218 the analyte from MRT Gel SPE columns.

219 *3.1.2* Selection of eluent and eluent concentration

220 The eluent should be able to extract the analyte without affecting the quantitative 221 determination of analytes (Chen et al., 2009). Analytes retained in the TE-01 and AN-01 SPE 222 columns were eluted with HNO₃ (4 mL) of varying concentrations (0.1–6.0 M). The recovery patterns were similar and the recovery rates became constant for the eluent concentration 223 224 above 0.5 M (Figs. 1a and 1b). However, greater than or equal to 5.0 M acids were recommended for the elution of bound ions in TE-01 and AN-01 SPE columns (IBC 225 226 Advanced Technologies, 2007, 2009). Hence, a combination of 1.0 M HNO₃ (2 mL) and 6.0 227 M HNO₃ (1 mL) was selected as eluent for the subsequent experiments to ensure the 228 complete elution of the analyte when treated with TE-01 or AN-01. On the other hand, only 229 0.1-4.0 M NaOH (2 mL) or 0.1-6.0 M HNO₃ (2 mL) was found unsuitable for the elution of 230 analytes from As-01. Combinations of 0.1-4.0 M NaOH (1 mL) followed by 2.0 M HNO₃ (1 231 mL) and vice-versa were used to check the elution of arsenic species from the As-01 column 232 (Figs. 1c and 1d). The recovery was achieved at quantitative maximum for the following 233 eluent combination: $0.1 \text{ M HNO}_3 (1 \text{ mL}) + 2.0 \text{ M NaOH} (1 \text{ mL})$, and was applied for the next 234 experiments with As-01 MRT gel column.

235 3.2 Retention behavior of the MRT gel SPE columns

The retention efficiency of the MRT gel SPE columns for different arsenic species at 236 237 varying pH is illustrated in Fig. 2. The retention (%) of As(III) was negligible with TE-01 and 238 AN-01 SPE columns. Average retention efficiency (%) of 92±3.7 was observed with As-01 239 column at the pH 4 to 10 while it was highest at pH 7 (96±1.2). As(III) mainly exists as a 240 neutral species, As(OH)₃, at the entire range of the studied pH. Thus, the macrocyclic 241 materials immobilized in the TE-01 and AN-01 columns were not capable of retaining the 242 neutral form of As(III). Almost complete retention of As(V) and MMA was achieved at pH 4 243 to 7 with all the MRT gel SPE columns. As(V) and MMA remain in the anionic form within that pH range, as evident from the corresponding pK_a values. Therefore, all of the MRT gel columns investigated can retain the anionic form of As(V) and MMA. DMA, which exists as a cation in the acidic medium, was retained at an average efficiency (%) of 94±3.3 with As-01 column between pH 4 and 6 while the retention was not that notable with TE-01 and AN-01 columns.

249 Data evaluation showed that the most significant finding of our work was with As(III). 250 Yu et al. (2003) checked 11 SPE systems at pH 5.6 and found that none of them were capable 251 of retaining As(III) quantitatively. Yalcin and Le (2001) worked with 7 SPE systems and 252 reported that Alumina-A, -B and -N (normal phase in acidic, basic, and neutral activity; from 253 Millipore-Waters, Missisauga, ON, Canada) and silica-based LC-SCX (sulfonic acid-bodned; 254 from Supelco, Bellefonte, PA, USA) columns can retain As(III) at the pH of 5.5. None of 255 those SPE systems were recommended for As(III) separation considering the difficulty in 256 elution. In our study, at pH 7, As(III) was completely retained at As-01 SPE column followed 257 by quantitative recovery.

258 3.3 Extraction and recovery behavior of the MRT gel SPE columns

The extraction behavior of the MRT gel SPE columns with four arsenic species is illustrated in Fig. 3. A similar extraction pattern was observed with TE-01 and AN-01 SPE columns; As(III) was not captured, As(V) was captured at an average rate (%) of 99 \pm 0.5 until pH 8, MMA extracted at an average percent rate of 99 \pm 0.60 at pH 6 and 7, and the highest extraction (%) of 71 \pm 4.6 was observed at pH 7 for DMA. With As-01 SPE columns, the average extraction (%) was 96 \pm 3.2 at pH 4–6 for As(V), MMA and DMA, while it was 99 \pm 1.1 at pH 7–9 for As(III).

Recovery (%) of the arsenic species with the MRT gel SPE columns is shown in Fig. 4. TE-01 SPE columns showed quantitative recovery performance at the entire studied pH range for all the arsenic species. AN-01 SPE columns showed similar behavior with As(III), As(V) and DMA while fluctuating recovery was achieved for MMA at different pH. A gradual increase in the recovery (%) was observed from pH 4 to pH 10 with As-01 SPE columns, and expected maximum recoveries were achieved for all the arsenic species at pH 7.

272 The extraction and recovery behavior of the MRT gel SPE columns leads us to the 273 following assumptions: (i) TE-01 and AN-01 columns are not effective for As(III) separation 274 but can be used to separate other target species (As(V), MMA and DMA) quantitatively at 275 varying pH conditions; (ii) selective separation and complete elution of As(III) is possible 276 with the As-01 column; (iii) the As-01 column can also be used to preconcentrate the targeted 277 water-soluble arsenic species for the determination of total arsenic content in the samples, if 278 selective separation is not desired; and (iv) column regeneration process is simple because the 279 retained analytes are completely eluted.

280 3.4 Interference studies

Cations of alkaline and alkaline earth metals are always found in water samples and have 281 282 the capability to compete with the target metal ions during the binding with the SPE material, 283 and common anions have the ability to bind with the target metal ions. In their presence, the 284 efficiency of the SPE material to bind the target ions may be reduced resulting in a reduction 285 of the recovery. The effects of matrix ions in water samples on the recovery of the spiked sample solutions of 100 µM As(III), As(V), MMA and DMA were investigated. The 286 recovery of different arsenic species in the presence of 10 mM of different ions (Na⁺, K⁺, 287 Ca^{2+} , Mg^{2+} , Cl^- , NO_3^- , CH_3COO^- , PO_4^{3-} , SO_4^{2-} , ClO_4^-) in the water samples were observed 288 289 in the range of $95\pm2.7-100\pm3.2\%$. Therefore, there is limited possibility of the interference 290 from the matrix ions commonly found in sample waters, which is may be due to the selective 291 separation capability of the MRT gel SPE materials.

292 **3.5** Retention capacity and regeneration of the SPE columns

293 Retention capacity of the MRT gel SPE columns is important for determining the stability of the MRT gel SPE columns during the separation process. Analyte concentration and 294 295 breakthrough volume (the volume of sample that causes the target analyte to be eluted from 296 the SPE columns) were used to find out the retention capacity (Yu et al., 2003). After arsenic-297 spiked sample solutions were passed through the SPE columns, the retention capacity was 298 expressed in terms of mmol of analyte captured in one gram of SPE material. The retention 299 capacities of the MRT gel SPE columns at pH 7 were calculated as follows: 0.40±0.02 mmol g^{-1} TE-01, 0.39±0.02 mmol g^{-1} AN-01 and 0.31±0.01 mmol g^{-1} As-01 (sample solution– 10 300 mM of As(V), matrix– H₂O, flow rate– 0.2 mL min⁻¹, elution– 2 mL of HNO₃ + 1 mL of 6 301 302 M HNO₃ + 1 mL of EPW, for TE-01 and AN-01 SPE columns and 1 mL of 0.1 M HNO₃ + 1 303 mL of 2.0 M NaOH + 2 mL of EPW). The result was in good agreement with the certified 304 values for the MRT gel SPE columns (IBC Advanced Technologies, 2006, 2007, 2009). The 305 regeneration ability of the MRT gel SPE columns was investigated, and it was observed that 306 more than 100 loading and elution cycles can be performed without the loss of analytical 307 performance. SPE systems with macrocycles attached onto solid supports allow selective 308 separation of analytes from matrix facilitating the repeated use of the macrocycles (Bradshaw 309 et al., 1988; Horwitz et al., 1992; Izatt, 1997).

310 **3.6** Scheme for selective separation of arsenic species

The differences in extraction and recovery pattern of MRT gel SPE columns for different arsenic species enabled us to propose a selective separation method. The method is based on the selective retention of the arsenic species followed by quantitative selective recovery at the elution step. Retention, extraction and recovery behavior of three MRT gel SPE columns: TE-01, AN-01 and As-01 were studied and combined to design a multi-step separation technique for quantitative measurement of As(III), As(V), MMA and DMA. Another MRT gel SPE column, AnaLig AN-02, was also checked. The retention, extraction and recovery behaviors of the AN-02 column were somewhat similar with those of AN-01 column. Therefore, AN-02 column can be considered as an alternative of AN-01 column in the separation process. The scheme for selective separation with subsequent quantitative measurement of the arsenic species by GF-AAS technique is shown in Fig. 5.

322 At pH 5, As(V) and MMA were quantitatively retained in the TE-01 SPE column while 323 As(III) and DMA remained in the column effluent. The captured species was eluted with 324 HNO₃. The eluted solution was separated into two equal portions, and pH was adjusted to 5 325 and 8 respectively. When each of the pH-adjusted portions independently treated with AN-01 326 SPE columns, As(V) and MMA were quantitatively extracted and recovered from the eluted solution, respectively, at pH 5 and pH 8. The column effluent containing As(III) and DMA 327 328 were adjusted to pH 9, and treated with As-01 SPE column. DMA remained in the solution 329 that passed through the SPE material while As(III) was selectively captured. Captured As(III) 330 was eluted with the eluent combination of 0.1 M HNO₃ followed by 2.0 M NaOH. GF-AAS were used to determine the concentration of the individual arsenic species. 331

332 **3.7** Analytical characteristics

333 The concentrations of As(III), As(V), MMA and DMA in the treated solutions from MRT gel SPE columns were measured using GF-AAS. At optimum conditions, the linear range 334 was found to be 0.01–0.32 μ g mL⁻¹ As(III), 0.01–0.78 μ g mL⁻¹ As(V), 0.01–0.35 μ g mL⁻¹ 335 MMA and 0.01–0.54 $\mu g m L^{-1}$ DMA. The method detection limits were calculated by three 336 times the standard deviation (n = 15) of the blank. The values were 0.06 µg L⁻¹ for As(III) 337 and As(V), and 0.05 μ g L⁻¹ for MMA and DMA. The precision of the method was also 338 339 studied. The repeatability, as relative standard deviation, was 0.65, 2.93, 2.25 and 1.20%, calculated from 10 replicate measurements at the 1.0 µM of As(III), As(V), MMA and DMA 340 341 respectively.

342 **3.8** Accuracy and applications

343 The accuracy of the proposed separation scheme was evaluated by analyzing two EC-344 JRC-IRMM CRMs, namely BCR-713 (effluent wastewater) and BCR-610 (groundwater) 345 (Table 3). None of the arsenic species measured in this work has either certified or literature 346 values. Our values for the total of all arsenic species determined for both BCR-713 and BCR-347 610 were in good agreement with the certified value, the calculated recoveries, 97% for BCR-348 713 and 94% for BCR-610, were satisfactory. The proposed separation scheme was also 349 applied to the analysis of local natural water samples (tap water and river water) and was 350 validated by spiking the samples with known amounts of As(III), As(V), MMA and DMA 351 (Table 4). The recoveries from spiked solutions were varied in the range $98 \pm 1.6 - 102 \pm 1.7\%$.

4.0 Conclusions

353 The application of three MRT gel SPE columns (TE-01, AN-01 and As-01) for selective 354 separation of four different arsenic species (As(III), As(V), MMA and DMA) was 355 demonstrated. Retention behaviors of the arsenic species were varied with the change of pH 356 at the range of 4 to10. TE-01 and AN-01 SPE columns were unable to retain As(III) while 357 As-01 showed the ability to retain all the species at a certain pH quantitatively. Either HNO₃ 358 or a combination of HNO₃ and NaOH were used as eluent to recover the 'captured' species 359 from the MRT gel structure. However, the recovery ratio was also found to depend on the pH. 360 pH-dependent retention and recovery behavior of the MRT gel SPE columns were used to 361 design a selective separation scheme for quantitative determination of a particular arsenic 362 species in the sample solution. It is possible to overcome the tedious preconcentration process 363 by following the proposed selective separation technique. To the best of our knowledge, it is 364 the first ever report dealing with SPE columns equipped with immobilized macrocyclic material as sorbent material for selective determination of arsenic in water. In addition, 365 quantitative retention followed by recovery of As(III) was achieved with As-01 column 366

367	which was previously not achieved with any other reported SPE systems. Easy operation,
368	virtually unlimited loading and elution capability of the sorbent material without losing the
369	analytical performance and high-sensitive separation ability can make the proposed technique
370	as a useful one for selective separation of arsenic species from natural waters.
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	Sten	Function	Solution	Volume	Flow rate
	Step	T unetion	Solution	(mI)	$(mI min^{-1})$
	1	Diaging 1			
	1	Rinsing I	0.1 M HNO ₃	8	0.5
	2	Rinsing 2	EPW	6	0.5
	3	Conditioning	$200 \text{ mM NaNO}_3 + 0.1 \text{ M buffer solution}^*$	32–40	0.2–0.5
	4	Collection	100 µM As-species spiked sample solution	4	0.2
	5	Washing	EPW	4	0.2
	6	Elution 1	For TE-01 or AN-01 SPE columns		
			1 M HNO ₃	2	0.2
			For As-01 SPE column		
			0.1 M HNO ₃	1	0.2
	7	Elution 2	For TE-01 or AN-01 SPE columns		
			6 M HNO ₃	1	0.2
			For As-01 SPE column		
			2.0 M NaOH	1	0.2
	8	Elution 3	For TE-01 or AN-01 SPE columns		
			EPW	1	0.2
			For As-01 SPE column		
			EPW	2	0.2
526	*MES B	uffer (pH 4–6), HEPE	ES Buffer (pH 7–8), TAPS Buffer (pH 9–10)		
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525	Table 1. Separation process of As(III), As(V), MMA and DMA using MRT gel SPE column	ns
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	Flow rate (mL min ⁻¹)	TE-01	AN-01	As-01
	0.20	101±3.8	100±3.7	101±4.6
	0.25	99±3.0	100±3.4	100±4.3
	0.30	88±2.8	82±2.6	92±3.8
	0.50	75±2.4	71±2.7	87±2.9
	1.00	74 ± 1.8	68±3.2	82±2.7
	2.00	65±2.6	62±1.6	71±3.4
	4.00	62±3.2	59±1.8	68±2.2
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535 Table 2. Effect of the sample loading flow-rates on the retention capacities (%) of the MRT

536 gel SPE columns

Arsenic species	Effluent Waste	ewater CRM	Groundwater	CRM
	BCR-713 (µg	L^{-1})	BCR-610 (µg	L^{-1})
	This work	Certified value	This work	Certified value
As(III)	1.9±0.3	NR	3.3±0.6	NR
As(V)	7.1±1.2	NR	6.9±1.1	NR
MMA	BDL	NR	BDL	NR
DMA	0.4 ±0.1	NR	BDL	NR
\sum (As-species)	9.4±1.4	9.7±1.1	10.2±1.6	10.8 ± 0.4
*'BDL' – Below Dete	ctable Limit; 'NR'-	Not reported		
	, -	I I I I I I I I I I I I I I I I I I I		

551 Table 3. Analysis of EC-JRC-IRMM CRMs for arsenic species

	Arsenic	Tap water			River water			
	species	Added	Found	Recovery	Added	Found	Recovery	
		$(\mu g L^{-1})$	$(\mu g L^{-1})$	(%)	$(\mu g L^{-1})$	$(\mu g L^{-1})$	(%)	
	As(III)	0	BDL	_	0	0.7±0.12	_	
		19.5	19.3±0.10	99±0.5	20	19.4±0.41	99±2.1	
	As(V)	0	BDL	_	0	1.3±0.15	_	
		31.2	31.3±0.48	100±1.5	31.2	30.5±0.51	98±1.6	
	MMA	0	BDL	_	0	BDL	_	
		21.0	21.3±0.34	102±1.7	21.0	20.7±0.43	99±2.0	
	DMA	0	BDL	_	0	0.1±0.01	_	
		32.1	32.3±0.27	101±0.8	32.1	31.9±0.60	99±1.9	
568	*'BDL' – Bela	ow Detectable	Limit					
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Table 4. Determination of arsenic species in the fortified samples of 'real' waters



Figure 1: Selection of eluent and eluent concentration: (a) AnaLig TE-01 (HNO₃-0.1/0.2/0.3/0.5/1.0/6.0 M) (b) AnaLig AN-01 Si (HNO₃- 0.1/0.2/0.3/0.5/1.0/6.0 M) (c) AnaLig As-01 PA (HNO₃- 0.1/1.0/2.0/4.0/6.0 M + NaOH- 2.0 M) (d) AnaLig As-01 PA (NaOH- 0.1/1.0/2.0/3.0/4.0 M + HNO₃- 2.0 M). Sample solution- As(V) (100 µM), matrix-H₂O, pH– 5, sample volume– 4 mL, flow rate– 0.2 mL min⁻¹ (n = 3).



Figure 2: Retention behavior of the MRT gel SPE columns. Sample solution– As(III), As(V), MMA and DMA (100 μ M), matrix– H₂O, pH– 4 to 10, sample volume– 4 mL, flow rate– 0.2 mL min⁻¹, elution– 1.0 M HNO₃ (2 mL) + 6.0 M HNO₃ (1 mL) + EPW (1 mL), for TE-01 and AN-01 SPE columns and 0.1 M HNO₃ (1 mL) + 2.0 M NaOH (1 mL) + EPW (2 mL), for As-01 SPE column (*n* =3).



Figure 3: Extraction behavior of the MRT gel SPE columns: (a) AnaLig TE-01, (b) AnaLig AN-01 Si and (c) AnaLig As-01 PA. Sample solution– As(III), As(V), MMA and DMA (100 μ M), matrix– H₂O, pH– 4 to 10, sample volume– 4 mL, flow rate– 0.2 mL min⁻¹, elution– 1.0 M HNO₃ (2 mL) + 6.0 M HNO₃ (1 mL) + EPW (1 mL), for TE-01 and AN-01 SPE columns and 0.1 M HNO₃ (1 mL) + 2.0 M NaOH (1 mL) + EPW (2 mL), for As-01 SPE column (*n* =3).



Figure 4: Recovery behavior of the MRT gel SPE columns: (a) AnaLig TE-01, (b) AnaLig AN-01 Si and (c) AnaLig As-01 PA. Sample solution– As(III), As(V), MMA and DMA (100 μ M), matrix– H₂O, pH– 4 to 10, sample volume– 4 mL, flow rate– 0.2 mL min⁻¹, elution– 1.0 M HNO₃ (2 mL) + 6.0 M HNO₃ (1 mL) + EPW (1 mL), for TE-01 and AN-01 SPE columns and 0.1 M HNO₃ (1 mL) + 2.0 M NaOH (1 mL) + EPW (2 mL), for As-01 SPE column (*n* =3).



Figure 5: Scheme for selective separation of the arsenic species by MRT gel SPE columns